

**Amendments to the Specification:**

Please replace the paragraph beginning on page 9, line 10 with the following rewritten paragraph:

--FIG. 5 schematically illustrates details of one example of an arrangement of surface 63, viewed from the front, *i.e.*, from inside delay loop 60, of graded reflectivity beamsplitter 62. Here, an arrangement suitable for three passes (round trips) in the delay loop 60 is depicted. At least three round trips is preferred. Three passes in delay loop 60 will provide four replica pulses 70A-D in an output beam as described above. Three passes are selected here for convenience of illustration. Those skilled in the art will recognize, without further illustration how beam 70 would propagate for four or more round trips providing, correspondingly, five or more pulse replicas. The greater the number of replicas, the greater the possible pulse extension. In a delay loop such as ~~delay loop 68~~, delay loop 60, the number of passes (and corresponding number of replica pulses) possible is limited only by the amount of loss of pulse energy that can be tolerated.--

Please replace the paragraph beginning on page 14, line 3 with the following rewritten paragraph:

--FIG. 10 schematically illustrates a second preferred embodiment 78 of a pulse extender in accordance with the present invention including a delay loop 80. Pulse extender 78 is similar to ~~extender 60~~ extender 58 of FIG. 4 with an exception that graded reflectivity beamsplitter 62 of pulse ~~extender 60~~ extender 58 is replaced by a graded reflectivity beamsplitter 65 in the form of a meniscus lens having zero dioptric power. Graded reflectivity zones are formed on concave surface 67 of the beamsplitter. Surface 67, considered as a mirror, has the same focal length  $f$  as mirrors 64, 66, and 68. Opposing mirrors are spaced by a distance of about  $2f$  such that 1:1 relay imaging conditions are satisfied. Providing that graded reflectivity beamsplitter 65 is a meniscus lens of zero power avoids the beamsplitter changing the divergence of transmitted replica pulses. It should be noted here that the sequence of graded reflectivity zones  $R_1$ ,  $R_2$ ,  $R_3$ , and  $R_4$  (not shown), of beamsplitter 65 must be arranged in the opposite sense to those of beamsplitter 62 depicted in FIG. 5.--